試題

系所組別:0330機械工程系碩士班丙組

科 目:熱力與流力

<<503302>>



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科 目:熱力與流力

- 1. (15%) Water flows steadily through a horizontal device as shown in Fig. 1. At the inlet 1 the diameter is D_1 =20 cm; at the outlet 2 the diameter is D_2 =10 cm. The flow rate is Q=0.02 m³/s. If the specific gravity (S.G.) of fluid in the U-tube is 11, what is the height difference Δh in the U-tube? Note that $\rho_{water} = 1,000 \text{ kg/m}^3$.
- 2. (10%) A ball is suspended in an air jet in a stable position as shown in Fig. 2. Experiments show that the equilibrium height, h, of the ball is found to depend on the ball diameter, D, and weight, W, jet diameter, d, and velocity, V, and the air density, ρ , and viscosity, μ .
 - (a) (2%) How many dimensionless parameters are obtained in this problem?
 - (b)(8%) Determine the dimensionless parameters that characterize this experiment.

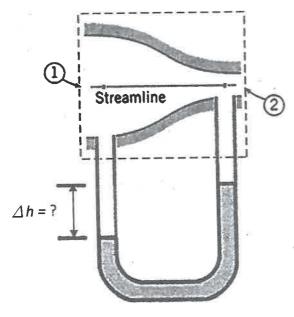


Fig. 1

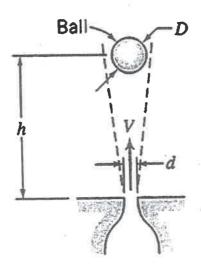


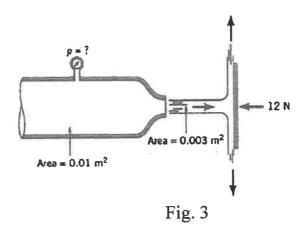
Fig. 2



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- 3. (15%) Air flows into the atmosphere from a nozzle and strikes a vertical plate as shown in Fig. 3. A horizontal force of 12 N is required to hold the plate in place.
 - (a) (10%) Determine the velocity strikes the vertical plate.
 - (b)(5%) Determine the reading on the pressure gage. The flow is assumed to be incompressible and frictionless.



$$(\mu_{\text{water}} = 1.2 \times 10^{-3} \text{ N} \cdot \text{s/m}^2, \rho_{\text{water}} = 1,000 \text{ kg/m}^3, \rho_{\text{air}} = 1.23 \text{ kg/m}^3, g = 9.8 \text{ m/s}^2, P_{\text{atm}} = 10^5 \text{ Pa})$$

- 4. (10%) For a two-dimensional flow field, the x and y velocity components are given by $u = 3x^2 3y^2$ and v = -6xy (unit: m/s), respectively. Please answer the following questions:
 - (a) (3%) Is it an incompressible flow? And why?
 - (b)(3%) Is the flow irrotational? And why?
 - (c) (4%) Please show the stream function for it.



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(總分為100分;所有試題務必於答案卷內頁依序作答)

5. (10%) True or False questions

- (a) (2%) Pressure is an extensive property because you can measure it externally.
- (b)(2%) Compressibility factor Z equals 1 for ideal gas.
- (c) (2%) Relative pressure $P_r \equiv \exp\left(\frac{s^\circ}{R}\right)$ is valid only in an isentropic process of an ideal gas.
- (d)(2%) If operating at the same temperature difference between the heat source and the heat sink, no real heat engine can have higher efficiency than a heat engine operating in a Carnot cycle.
- (e) (2%) In an adiabatic process, the system exchanges no heat with its surroundings.

6. (10%) Single choice questions

- (a) (2%) Which of the following mechanisms cannot transfer entropy? A. heat convection, B. mass flow, C. heat radiation. and D. work across system boundaries.
- (b)(2%) A common approximation for calculating the properties of the compressed liquid without precise compressed liquid data, such as the property tables, is to treat compressed liquid as saturated liquid at the given temperature. This is because the compressed liquid properties change more quickly with A. pressure, B. temperature, C. specific volume, and D. none of the above.
- (c) (2%) In a steady-flow throttling process of an ideal gas, which of the following properties changes? A. pressure, B. enthalpy, C. temperature, and D. mass flow rate.
- (d)(2%) Which process requires the most work for a compression process operating at the same pressure limits? A. isothermal process, B. polytropic process, C. isentropic process, and D. none of the above.
- (e) (2%) Which steady-flow device cannot be isentropic even for an ideal situation? A. a compressor, B. a turbine, C. a nozzle, and D. a mixing chamber of two fluids at different temperatures.

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- 7. (10%) A heat engine operates between two reservoirs at 700°C and 5°C. Two-thirds (2/3) of the work output of the heat engine is used to drive a heat pump that removes heat from a cold surrounding at 5°C and transfers it to a house maintained at 20°C. If the house's heat loss is at a rate of 50000 kJ/h, please answer the following questions.
 - (a) (2%) Calculate the coefficient of performance of the heat pump.
 - (b)(2%) Calculate the thermal efficiency of the heat engine.
 - (c) (4%) Determine the minimum rate of heat supply to the heat engine to keep the house temperature maintained at 20°C if the heat pump is operating at a Carnot cycle.
 - (d)(2%) The actual coefficient of performance of the heat pump and the thermal efficiency of the heat engine are 3.5 and 30%, respectively. Is setting up such a system still more energy efficient than a direct electric heating system? Explain your reason by calculations.
- 8. (10%) A horizontal cylinder is separated into two compartments by an adiabatic, frictionless piston, as shown in Fig. 8. One side contains 0.4 m^3 of nitrogen and the other side contains 0.1 kg of helium, both initially at 25°C and 101kPa. The sides of the cylinder and the helium end are insulated. Now heat is added to the nitrogen side from a heat reservoir at 500 °C until the pressure of the helium rises to 150 kPa. Please answer the following questions:
 - (a) (2%) Determine the final temperature of the helium.
 - (b)(2%) Determine the final volume of the nitrogen.
 - (c) (3%) What is the heat transferred to the nitrogen?
 - (d)(3%) The entropy generation during this process.

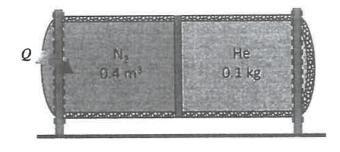


Fig. 8



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(總分為100分;所有試題務必於答案卷內頁依序作答)

Table 1

(e) At 300 K									
Gas	Formula	Gas constant, R kJ/kg K	c _n kJ/kg⋅K	c, kJ/kg-K	<u>k</u>				
Av		0.2870	1.005	0.718	1.400				
Argon	Ar	0.2081	0.5203	0.3122	1.667				
Butane	C ₄ H ₇₀	0.1483	1.7164	1.5784	1.091				
Carbon dioxide	CO ₂	0.1889	0.846	0.657	1.289				
Carbon monoxide	co	0.2968	1 040	0.744	1.400				
Ethane	C ₂ H ₆ .	0.2765	1.7662	1,4897	1.186				
Ethylene	C ₂ H _A	0.2964	1.5482	1.2518	1.237				
Hellum	He	2.0759	5.1926	3,1156	1,667				
THE RESIDENCE OF THE PROPERTY	Ha	4.1240	14.307	10.183	1,405				
Hydrogen	OH _a	0.5182	2.2537	1.7354	1.299				
Methane	Ne	0.4119	1.0299	0.6179	1.667				
Neon	N ₂	0.2968	1 039	0.743	1.400				
Nitrogen	C ₈ H ₁₈	0.0729	1.7113	1,6385	1,044				
Octane		0.2598	0.918	0.668	1,395				
Oxygen	O ₂ C ₃ H ₈	0.1885	1.6794	1.4909	1.126				
Propane Steam	H ₂ O	0.4615	1.8723	1.4108	1.327				

Note: The unit kJ/kg·K is equivalent to kJ/kg·°C.

Source of Data: B. G. Kyle, Chemical and Process Thermodynamics, 3rd ed. (Upper Saddle River, NJ: Prentice Hall, 2000).

- 9. (10%) An isentropic steam turbine processes $3.5 \, kg/s$ of steam at 4 MPa, and 90% of the flow is used to generate power and exhausted at 50 kPa and 100°C. The rest of the steam mass flow is diverted and mixed with the feedwater in a mixing chamber for preheat, which exits the turbine at 800 kPa. Please answer the following questions:
 - (a) (5%) Determine the power produced by this turbine in kW.
 - (b)(3%) If the turbine has an isentropic efficiency of 90%, determine the power produced by this turbine in kW.
 - (c) (2%) If the feedwater at the mixing chamber inlet is at 20°C, 800 kPa, and leaves the mixing chamber as a saturated liquid. Assuming the turbine is still isentropic, determine the maximum mass flow rate of feedwater that can be preheated. Is this process reversible? Why?



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Table 2

		Specific volume, m³/kg		Inte	Internal energy, kJ/kg			Enthalpy, kJ/kg			Entropy, kJ/kg-K		
Temp.,	Sat. press., P _{sat} kPa	Sat. liquid, v,	Sat vapor,	Sat. liquid, u,	Evap.,	Sat. vapor, u _g	Sat. liquid, h _f	Evap.,	Sat. vapor, h _g	Sat. liquid,	Evap.,	Sat. vapor, s _g	
0.01 5 10 15 20	0.6117 0.8725 1.2281 1.7057 2.3392	0.001000 0.001000 0.001000 0.001001 0.001002	206,00 147,93 106,32 77,885 57,762	0.000 21.019 42.020 62.980 83.918	2374.9 2360.8 2346.6 2332.5 2318.4	2374.9 2381.8 2388.7 2395.5 2402.3	0.001 21.020 42.022 62.982 83.915	2500.9 2489.1 2477.2 2465.4 2453.5	2500.9 2510.1 2519.2 2528.3 2537.4	0:1511 0:2245	9.1556 8.9487 8.7488 8.5559 8.3696	9,024 8,899 8,780	
25 30 35 40 45	3.1698 4.2469 5.6291 7.3851 9.5953	0.001003 0.001004 0.001006 0.001008 0.001010	43.340 32.879 25.205 19.515 15.251	104.83 125.73 146.63 167.53 188.43	2304.3 2290.2 2276.0 2261.9 2247.7	2409.1 2415.9 2422.7 2429.4 2436.1	104.83 125.74 146.64 167.83 188.44	2441.7 2429.8 2417.9 2406.0 2394.0	2546.5 2555.6 2564.6 2573.5 2582.4	0.3672 0.4368 0.5051 0.5724 0.6386	8.1895 8.0152 7.8466 7.6832 7.5247	8.452 8.351 8.255	
50 55 60 65 70	12.352 15.763 19.947 25.043 31.202	0.001012 0.001015 0.001017 0.001020 0.001023	12.026 9.5639 7.6670 6.1935 5.0396	209.33 230.24 251.16 272.09 293.04	2233.4 2219.1 2204.7 2190.3 2175.8	2442.7 2449.3 2455.9 2462.4 2468.9	209.34 230.26 251.18 272.12 293.07	2382.0 2369.8 2357.7 2345.4 2333.0	2591.3 2600.1 2608.8 2617.5 2626.1	0.7036 0.7680 0.8313 0.8937 0.9551	7.3710 7.2218 7.0769 6.9360 6.7989	7.989 7.908 7.829	
75 80 85 90 95	38.597 47.416 57.868 70.183 84.609	0.001026 0.001929 0.001032 0.001036 0.001040	4.1291 3.4053 2.8261 2.3593 1.9808	313,99 334,97 355,96 376,97 398,00	2161.3 2146.6 2131.9 2117.0 2102.0	2475.3 2481.6 2487.8 2494.0 2500.1	314.03 335.02 356.02 377.04 398.09	2820.6 2808.0 2295.3 2282.5 2269.6	2634.6 2643.0 2651.4 2659.6 2667.6	1.0158 1.0756 1.1346 1.1929 1.2504	6.6655 6.5355 6.4089 6.2853 6.1647	7.611 7.543 7.478	
100 105 110 115 120	101.42 120.90 143.38 169.18 198.67	0.001043 0.001047 0.001052 0.001056 0.001060	1.6720 1.4186 1.2094 1.0360 0.89133	419.06 440.15 461.27 482.42 503.60	2087.0 2071.8 2056.4 2040.9 2025.3	2506.0 2611.9 2517.7 2523.3 2528.9	419.17 440.28 461.42 482.59 503,81	2256.4 2243.1 2229.7 2216.0 2202.1	2675.6 2683.4 2691.1 2698.6 2706.0	1.3072 1.3634 1.4188 1.4737 1.5279	5.7092	7.295 7.238	
125 130 135 140 145	232.23 270.28 313.22 361.53 415.68	0.001065 0.001070 0.001075 0.001080 0.001085	0.77012 9.66808 0.58179 0.59850 0.44600	524.83 546.10 567.41 588.77 610.19	2009.5 1993.4 1977.3 1960.9 1944.2	2534.3 2539.5 2544.7 2549.6 2554.4	525.07 546.38 567.75 589.16 610.64	2188.1 2173.7 2159.1 2144.3 2129.2	2713.1 2720.1 2726.9 2733.5 2739.8	1.5816 1.6346 1.6872 1.7392 1.7908	5.3919 5.2901 5.1901	7.077 7.026 6.977 6.929 6.887	
150 155 160 165 170	476.16 543.49 618.25 780.93 792.18	0:001091 0:001096 0:001102 0:001108 0:001114	0.39248 0.34648 0.30680 0.27244 0.24260	631.66 653.19 674.79 696.46 718.20	1927.4 1910.3 1893.0 1875.4 1857.5	2559.1 2563.5 2567.8 2571.9 2575.7	632.18 653.79 675.47 697.24 719.08	2113.8 2098.0 2082.0 2065.6 2048.8	2745.9 2751.8 2757.5 2762.8 2767.9	1.8418 1.8924 1.9426 1.9923 2.0417	4,9002 4,8066 4,7143	6.833 6.796 6.749 6.700 6.669	
175 180 185 190 195 200	892.60 1002.8 1123.5 1255.2 1398.8 1554.9	0.001121 0.001127 0.001134 0.001141 0.001149 0.001157	0.19384 0.17390 0.15636 0,14089	740.02 761.92 783.91 806.00 828.18 850.46	1839.4 1820.9 1802.1 1783.0 1763.6	2582.8 2586.0 2589.0	741.02 763.05 785.19 807.43 829.78 852.26	2031.7 2014.2 1996.2 1977.9 1959.0 1939.8	2772.7 2777.2 2781.4 2785.3 2788.8 2792.0	2.2355 2.2831	4.4441 4.357 4.270	6,54 6,50 7 6,46	



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Table 3

		Specific volume, m³/kg		Int	ernal ener k#/kg	gy,	Enthalpy, k#kg			Entropy, kJ/kg·K			
Press., P kPa	Sat. temp., T _{set} °C	Sat. Hquid,	Sat. vapor,	Sat. Ilquid.	Evap.,	Sat vapor, v _e	Sat. liquid, h _i	Evap.,	Sat. vapor, h _g	Sat. liquid,	Evap.,	Sat. vapor,	
1.0 1.5 2.0 2.5 3.0	6.97 13.02 17.50 21.08 24.08	0.001900 0.001901 0.001901 0.001002 0.001003	129.19 87.964 66.990 54.242 45.654	29.302 54.686 73.431 88.422 100.98	2355.2 2338.1 2325.5 2315.4 2306.9	2384.5 2392.8 2398.9 2403.8 2407.9	29.303 54.668 73.493 88.424 100.98	2484.4 2470.1 2459.5 2451.0 2443.9	2513,7 2524,7 2532,9 2539,4 2544,8	0.1059 0.1956 0.2606 0.3118 0.3543	8.8690 8.6314 8.4621 8.3302 8.2222	8,9749 8,8270 8,7227 8,6421 8,5765	
4.0 5.0 7.5 10	28.96 32.87 40.29 45.81 53.97	0:001004 0:001005 0:001008 0:001010 0:001014	34.791 28.185 19.233 14.670 10.020	121.39 137.75 168.74 191.79 225.93	2293.1 2282.1 2261.1 2245.4 2222.1	2414.5 2419.8 2429.8 2437.2 2448.0	121.39 137.75 168.75 191.81 225.94	2432.3 2423.0 2405.8 2392.1 2372.3	2560.7 2574.0 2583.9	0.4224 0.4762 0.5763 0.6492 0.7549	7.4996 7.2522	8.4734 8.3938 8.2501 8.1488 8:0071	
20 25 30 40 50	60.06 64.96 69.09 75.86 81.32	0.001017 0.001020 0.001022 0.001026 0.001030	7.6481 6.2034 5.2287 3.9983 3,2403	251.40 271.93 289.24 317.58 340.49	2204.6 2190.4 2178,5 2158.8 2142.7	2456.0 2462.4 2467.7 2476.3 2483.2	251,42 271,96 289,27 317,62 340,54	2357.5 2345.5 2335.3 2318.4 2304.7	2608.9 2617.5 2624.6 2636.1 2645.2	0.8932 0.9441 1.0261	7.0752 6.9370 6.8234 6.6430 6.5019		
75 100 101.32! 125 150	91.76 99.61 5 99.97 108.97 111.35	0.001037 0.001043 0.001043 0.001048	1.3750	384,36 417,40 418,95 444,23 466,97	2111.8 2088.2 2087.0 2068.8 2052.3	2496.1 2505.6 2506.0 2513.0 2519.2	384.44 417.51 419.06 444.36 467.13	2278.0 2257.5 2256.5 2240.6 2226.0	2662.4 2675.0 2675.6 2684.9 2693.1	1.3069	6.2426 6.0562 6.0476 5.9100 5.7894	7.3589 7.3545 7.2841	
17.5 200 225 250 275	116.04 120.21 123.97 127.41 130.58	0.001057 0.001061 0.001064 0.001067 0.001070	0.88678 0.79329 0.71873	520.47 535.08	2087.7 2024.6 2012.7 2001.8 1991.6	2524.5 2529.1 2533.2 2536.8 2540.1	487.01 504.71 520.71 535.35 548.86	2213.1 2201.6 2191.0 2181.2 2172.0	2700.2 2706.3 2711.7 2716.5 2720.9	1.5302 1.5706 1.6072	5.5968 5.5171 5.4453	7.1270 7.0877 7.0528	
300 325 350 375 400	138.52 136.27 138.86 141.30 143.61	0.001076 0.001076 0.001079 0.001083	0.60582 0.56199 0.52422 0.49133	561.11 572.84 583.89 594.32	1982.1 1973.1 1964.6 1956.6 1948.9	2650.9	561.43 573.19 584.26 594.73 604.66	2163.5 2155.4 2147.7 2140.4 2133.4	2735.1	1.7005 1.7274 1.7526	5.2645 5.2128 5.164!	6.9402 5 6.9171	
450 500 550 600 650	147.90 151.83 155.46 158.83 161.98	0.00108 0.00109 0.00109 0.00110	8 0.41392 8 0.37483 7 0.34261 1 0.31560	622.65 639.54 655.16	1984.5 1921.2 1908.8 1897.1 1886.1	2557.1 2560.7 2569.9 2566.8	623.14 640.09 655.77 670.38 684.08	2120.3 2108.0 2096.6 2085.8 2075.8	2748. 2752. 2756.	1.8604 1.8970 2 1.9300 5 1.9620	4.960 4.891 3 4.828 3 4.769	6.820 6 6.788 5 6.759 9 6.732	
700 750	164.95 167.75	0.00110	8 0.2727	CONTRACTOR STATES	1875.6 1865.6			2065.8 2056.4		8 1.991 7 2.019	8 4.715 5 4.664		



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Table 4

		Specific volume, m³/kg		Internal energy, kJ/kg			Enthalby, kJ/kg			Entropy, kJ/kg-K		
Press., P kPa	Sat. temp., T _{sat} °C	Sat. liquid,	Sat. vapor,	Set. liquid, u,	Evap.,	Sat. vapor,	Sat. liquid, h,	Evap.,	Sat: vapor, h _e	Sat. liquid, s,	Evap.,	Sat. vapor,
800	170.41	0.001115	0.24035	719.97	1856.1	2576:0	720.87	2047.5	2768.3	2.0457	4.6160	6.661
850	172.94	0.001118	0.22690	731.00	1846.9	2577.9	731.95	2038.8	2770.8	2.0705	4.5705	6.640
900	175.35	0.001121	0.21489	741,55	1838.1	2579.6	742.56	2080.5	2773.0	2.0941	4.5273	6.621
950	177.66	0.001124	0.20411	751.67	DESCRIPTION OF A PARTY	2581.3	752.74	2022.4	2775.2	2.1166	4.4862	6,602
1000	179.88	0.001127	0.19436	11U(9)=M(22)-Z2L	1821.4	2582.8	762.51	2014.6	2777.1	2.1381	4.4470	6.585
1100	184.06	0:001133	0.17745	779.78	1805.7	2585.5	781.03	1999.6	2780.7	2.1785	4.3735	6.552
1200	187.96	0.001138	0.16326		1790.9	2587.8	798.33	1985.4	2783.8	2.2159	4.3058	6.521
1300	191.60	0.001144	0.15119	813.10	Note a south for	2589.9	814.59	1971.9	2786.5	2.2508	4,2428	6.493
1400	195.04	0.001149	0.14078		1763.4	2591.8	829.96	1958.9	2788.9	2.2835	4.1840	6.467
1500	198.29	0.001154	0.13171	842.82		2593.4	844.55	1946.4		2.3143	4.1287	6,443
1750	205.72	0.001/166	0.11344	876.12		2596.7	878.16	1917.1	2795.2	2.3844	4.0033	6.387
2000	212.38	0.001177	0.099587		1693.0	2599.1	908.47	1889,8	2798.3	2.4467	3.8923	6,339
2250	218.41	0.001187	0.088717	933.54	1667.3	2600.9	936.21	1864.3	2800.5	2.5029	3.7926	6.295
2500	223.95	0.001197	0.079952	958.87	1643.2	2602.1	961.87	1840.1	2801.9	2.5542	3.7016	6.255
3000	238.85	0.001217	0.066667	1004.6	1598.5	2603.2		1794.9	2803.2	2.6454	3.5402	6.185
3500	242.56	0.001235	0:057061	1045.4	1557.6	2603.0		1753.0	2802.7	2.7253	3:3991	6.124
4000	280.35	0.001253	0.037001	1082.4	1519.3	2601.7	AP DOMESTIC TO A PERSON	1713.5	2800.8	2.7966	3.2731	6.069
5000	263.94	0.001286	0.039448	1148.1	1448.9	2597.0	23 E S S S S S S S S S S S S S S S S S S	1639.7	2794.2	OF THE STREET, SALES	3.0530	5.973
6000	275.59	0.001319	0.032449	1205.8	1384.1	2589.9	80/2000/04/05/2010	1570.9	2784.6	3.0275	2.8627	5.890
7000	285.88	0.001352	0.027378	1258.0	1323.0	2581.0	MONROW HILL IN THE SET OF	1505.2	2772.6	3.1220	2.6927	5.814
8000	295.01	0.001384	0.023525	1306,0	1264.5	2570.5	1317.1	1441.6	2758.7	3.2077	2.5373	5.745
9000	308,35	0.001418	0.020489	1350:9	1207.6	2558.5	ACRES OF SECURITY ASK	1379.3	2742.9	3.2866	2.3925	5.679
10,000	311,00	0.001452	0.018028	1393.3	1151.8	2545.2	ASSESSMENT AND ADMINISTRATION OF THE PARTY O	1317.6	27.25,5		2.2556	5.615
11.000	318.08	0.001488	0.015988	1433.9	1096.6	2530.4		1256.1	2706.3	3,4299	2.1245	5.554
12,000	324.68	0.001526	0.014264	1473.0	1041.3	2514.3	SECURITY TO SECURE	1194.1	2685.4	3.4964	1.9975	5.493
13,000	330.85	0.001666	0.012781	1511.0	985.5	2496.6	1531.4	1131.3	2662.7	3.5606	1.8730	5.433
14,000	336.67	0.001610	0.011487	1548.4	928.7	2477.1	1571.0	1067.0	2637.9	3.6232	1.7497	5,372
15,000	342.16	0.001657	0.010341	1585.5	870.3	2455.7		1000.5	2610.8	3.6848	1.6261	5.310
16,000	347.36	0.001710	0.009812	1622.6	809.4	2432.0	1649.9	931.1	2581.0	3.7461	1.5005	5.246
17,000	352,29	0.001770	0,008374	1660.2	745.1	2405.4	1690.3	857.4	2547.7	3.8082	1.3709	5.179
18,000	356.99	0.001840	0.007504	1699.1	675.9	2375.0	1732.2	777.8	2510.0	3.87.20	1.2343	5.106
19,000	361.47	0.001926	0.006677	1740.3	598.9	2339.2	1776.8	689.2	2466.0	3.9396	1.0860	5.025
20,000	365.75	0.002038	0.005862	1785.8	509.0	2294.8	1826.6	585.5	2412.1	4.0146	0.9164	4:93
21,000	369.83	0.002207	0.004994	1841.6	391.9	HERMONIA PROPERTY	1888.0	450.4	2338.4	4.1071	0.7005	4.807
22,000	373.71	0.002703	0.003644	1951.7	140.8	2092.4	2011.1	161.5	2172.6	4.2942	0.2496	4.545
22,064	373.95	0.003106	0.003106	2015.7	0	2015.7	2084.3	0	2084.3	4,4070	0	4,40



系所組別:機械工程系碩士班丙組

目:熱力與流力

Table 5

Superh	eated wate	r		HE SHARE								
T	V	U	h	S	V	U	h	5	V	U t/13tem	PROFESSORS	S b UV= V
°C	m³/kg	kJ/kg	kJ/kg	kJ/kg-K	m³/kg	kJ/kg	kJ/kg	kJ/kg·K	m³/kg	kJ/kg	and the same of the last	kJ/kg/K
	P =	0.01 MP	a (45.81°C))=	P =	0,05 MPa	(81.32°	Q)	AND RESIDENCE AND RESIDENCE	= 0.10 MI	NUE DINE NO	Charles and Allen
Sat.†	14.670		2583.9	8.1488	3.2403	2483.2	2645.2	7.5931	1.6941	2505.6	2675.0	7.3589
50	14.867		2592.0	8.1741			The st			0505.0	0275.0	7 00 1
100	17.196	12000	2687.5	8.4489	3.4187	2511.5	2682.4	7.6953	1.6959		2675.8	7.3611
150	19.513	2587.9	2783.0	8.6893	3.8897	2585.7	2780.2	7.9413	1.9367	2582.9 2658.2	2776.6 2875.5	7.6148 7.8356
200	21.826	2661.4		8.9049	4.3562	2660.0	2877.8	8.1592 8.3568	2.1724 2.4062	2733.9	2974.5	8.0346
250	24.136	2736.1		9.1015	4.8206 5.2841	2735.1 2811.6	2976.2 3075.8	8.5387	2.6389	2810.7	3074.5	8.2172
300	26.446	2812.3 2969.3		9.2827 9.6094	6.2094	2968.9	3279,3	8.8659	3.1027		3278.6	8.5452
400 500	31.063 35.680	3132.9	3489.7	9.8998	7.1338	3132.6	3489.3	9.1566	3.5655		3488.7	8.8362
600	40.296	3303.3	3706.3	10.1631	8.0577	3303.1	3706.0	9,4201	4.0279		3705.6	9.0999
700	44,911	3480.8	OCUPRIOR STATE OF	10.4056	8.9813	3480.6	3929.7	9.6626	4.4900		3929.4	
800	49.527		4160.6		9.9047	3665.2	4160.4	9.8883	4.9519	3665.0	4160.2	9.5682
900	54.143	3856.9	Committee of the Commit	10.8429	10.8280	3856.8	4398.2	10.1000	5.4137	3856.7	4398.0	
1000	58.758		4642.8		11.7513	4055.2	4642.7	10.3000	5.8755		4642.6	MATERIAL PROPERTY OF THE PARTY
1100	63.373			11.2326	12.6745	4259.9	4893.7	10.4897	6.3372		STORUS CAR PORT	10.1698
1200	67.989			11.4132	13.5977	4470.8	5150.7	10.6704	6.7988	4470.7		10.3504
1300	72.604		5413.4		14.5209	4687.3	5413.3	10.8429	7,2605	4687,2	5413.3	10.5229
	ρ:	= 0.20 M	Pa (120.2	1°C)	P=	0.30 MP	a (133,6)	2°C)	P	= 0.40 Mf	Pa (143.6	1°C)
Sat.	0.88578	-	2706.3	7.1270	0.60582	2543.2	2724.9	6.9917	0.4624	2 2553.1	2738.1	6.8955
150	0.95986		2769.1	7.2810	0.63402		2761.2	CARL COLORS TO SERVICE	0.4708	8 2564.4	2752.8	6.9306
200		2654.6		7.5081	0.71643		2865.9		0.5843	4 2647.2	2860.9	7.1723
250			2971.2	7.7100	0.79645	TENEST PROPERTY.	2967.9	CORRESPONDED TO STATE OF THE PARTY OF THE PA	0.5952	0 2726.4	2964.5	7.3804
300		2808.8		7.8941	0.87585		3069.6		0.6548	9 2805.1	3067.1	7.5677
400			3277.0	8.2236	1.03155		3275.5		0.7726	5 2964.9	3273.9	
500			3487.7	8.5153	1.18672		3486.6	8.3271		6 3129.8	3485.5	
600			3704,8	8.7793	1.34189	3301.6	3704.0	8.5915		8 3301.0		
700			3928.8	9.0221		3479.5	3928,2			2 3479.0		WARRY TO SELECTION OF SELECTION
800	ALTERNATION OF THE PERSON NAMED IN COLUMN		4159.8			3664.3	4159.3		THE RESERVE AND ADDRESS OF THE PARTY AND ADDRE	0 3663.9	THE RESERVE OF THE PARTY OF	
900	2.70656	3856.3	4397.7	9.4598		3856.0	4397.3		N. SOU SHOWINGSON	8 3855.7	ENCORP. SET AND SET	
1000	2,9375	4054.8	4642.3			4054.5	4642.0			9 4054.3		GENERAL PROPERTY AND ADDRESS OF THE PARTY AND
1100	3.16848	4259.6		9.8497	2.11226		4893.1	COLUMN COMPANIES COMES		4 4259.2		
1200		AND RESIDENCE.	5 5150.4			4470.3	5160.2			6 4470.2		
1300	3.6302	4 68 7	1 5413,1	10.2029	2.42019	4686.9	5413.0	10.0157		6 4686.7	CALCUMITE IN	MERCHOONSE
	P	= 0,50 N	MPa (151.8	33°C)	P	= Q.60 M	Pa (158.8	(0°88)	A STATE OF THE PARTY OF THE PAR	= 0.80 M	OF STREET STREET	
Sat.	0.3748	3 2560.	7 2748.1	6,8207	0.31560	2566.8	2756.			35 2576.0		
200	0.4250	3 2643.	3 2855,8					6.9683	11 1976/05/05/05/05/05	38 2631.1		8 6.817
250	0.4744	3 2723.	8 2961.0	7.2725	STATE OF THE PARTY	2721.2				21 2715.9		
300			3 3084.6		AND THE PROPERTY OF THE PARTY O	2801.4			A DESCRIPTION OF THE PERSON NAMED IN	16 2797.5	Q16-50-305-722HES	CONTRACTOR AND
350			0 3168.1			3 2881.6		AACAMPT BUT LANDING TO		42 2878 6		
400			7 3272.4			2962.5				29 2960.2		
500			0 3484.9		AND RESIDENCE AND ADDRESS OF THE PARTY OF TH	3128.2		CARL PARTIES OF THE PARTY	0.443	32 3126.6 86 3298.7	3481. 3700.	
600	NUMBER OF STREET		4 3702.5			3299.8				86 3298.7 11 3477.2		COLUMN SECTION AND ADDRESS OF THE PARTY.
7.00	A STATE OF THE PARTY OF THE PAR		6 3927.0		MATERIAL STREET, THE PROPERTY OF	3478.1			DESCRIPTION OF THE PROPERTY.	20 3662.5	Brown Charles	THE PERSON NAMED IN
808	Marie Control of the		6 4158.			3663.2		SECTION AND PARTY OF THE PARTY OF	0.00 4660555462455	19 3854.5	MARKET SERVICE	SECURITIES TO THE PROPERTY OF
90	5793-54F120V120-4820V3-5		4 4396.		MAN BURGET TO MAKE HOWEVER	9 3855.1			SCT TAUDITHE PRO-	11 4053.3	Charles and Control of the	DESCRIPTION OF THE PROPERTY OF
100	AND A STATE OF THE PERSON NAMED IN		0 4641.		CONTRACTOR AND AND ADDRESS OF THE PARTY OF T	3 4053.8	PROPERTY AND ADDRESS OF THE	THE RESERVE OF THE PARTY OF THE	Control of the Contro	97 4258.5	STATE OF THE PARTY	MERICENZACION
110			0 4892.			3 4258.8		DESCRIPTION OF THE PERSON NAMED IN	CONTRACTOR OF THE PARTY OF THE	80 4469.4	SHEET STATE OF THE	\$200 BBC \$400 WE WITH \$100
120	CHARLES AND		0 5149.		NAME OF TAXABLE PARTY.	9 4469.8			ON CONTRACTOR AND	61 4686.		
130	0 1.4521	4 4686	.6 5412.	6 9.7797	1.2101	2 4686.4	+ 3412	19 310380	0.507	O4 7000.	grant (Arthur	,E 51001

^{*}The temperature in parentheses is the saturation temperature at the specified pressure.

† Properties of saturated vapor at the specified pressure.



系所組別:機械工程系碩士班丙組

科 目:熱力與流力

(總分為100分;所有試題務必於答案卷內頁依序作答)

Table 5 (Continued)

0.04978 0.05461 0.05887 0.06647 0.07343 0.08004 0.09886 0.11098 0.12292 0.13476 0.14653 0.16824 0.16992	2601.7 2668.9 2726.2 2827.4 2920.8 3011.0 3100.3 3279.4 3462.4 3650.6 3844.8 4045.1	250.35% 2800.8 2887.3 2961.7 3098.3 3214.5 3831.2 3446.0 3674.9 3906.3	6.0696 6.2312 6.3639 6.5843 6.7714 6.9386 7.0922	m ³ /kg P = 0.04406 0.04733 0.05138 0.05842 0.06477 0.07076	2599.7 2651.4 2713.0 2818.6	(257.44°0 2798.0 2864.4 2944.2	6.0198 6.1429	0.03945 0.04144	5,0 MPa ((268.94° 2794.2	5.9737
0.04978 0.05461 0.05887 0.06647 0.07343 0.08004 0.09886 0.11098 0.12292 0.13476 0.14653 0.16824 0.16992	2601.7 2668.9 2726.2 2827.4 2920.8 3011.0 3100.3 3279.4 3462.4 3650.6 3844.8 4045.1	2800.8 2887.3 2961.7 3098.3 3214.5 3831.2 3446.0 3674.9	6.0696 6.2312 6.3639 6.5843 6.7714 6.9386	0.04406 0.04733 0.05138 0.05842 0.06477	2599.7 2651.4 2713.0 2818.6	2798.0 2864.4	6.0198 6.1429	0.03945 0.04144	2597.0	2794.2	5.9737
0.04978 0.05461 0.05887 0.06647 0.07343 0.08004 0.09886 0.11098 0.12292 0.13476 0.14653 0.16824 0.16992	2601.7 2668.9 2726.2 2827.4 2920.8 3011.0 3100.3 3279.4 3462.4 3650.6 3844.8 4045.1	2800.8 2887.3 2961.7 3098.3 3214.5 3831.2 3446.0 3674.9	6.0696 6.2312 6.3639 6.5843 6.7714 6.9386	0.04406 0.04733 0.05138 0.05842 0.06477	2599.7 2651.4 2713.0 2818.6	2798.0 2864.4	6.0198 6.1429	0.04144	A STATE OF THE PARTY OF THE PAR		24.0e51.0e5271.74551
0.05461 0.05887 0.06647 0.07343 0.08004 0.08644 0.09886 0.11098 0.12292 0.13476 0.14653 0.15824 0.16992	2668.9 2726.2 2827.4 2920.8 3011.0 3100.3 3279.4 3462.4 3650.6 3844.8 4045.1	2887.3 2961.7 3098.3 3214.5 3331.2 3446.0 3674.9	6.2312 6.3639 6.5843 6.7714 6.9386	0.04733 0.05138 0.05842 0.06477	2651.4 2713.0 2818.6	2864.4	6.1429	0.04144	A STATE OF THE PARTY OF THE PAR		24.0e51.0e5271.74551
0.05887 0.06647 0.07343 0.08004 0.08644 0.09886 0.11098 0.12292 0.13476 0.1663 0.16824 0.16992	2726.2 2827.4 2920.8 3011.0 3100.3 3279.4 3462.4 3650.6 3844.8 4045.1	2961.7 3098.3 3214.5 3331.2 3446.0 3674.9	6.3639 6.5843 6.7714 6.9386	0.05138 0.05842 0.06477	2713.0 2818.6	CANNERS DECIPION	THE PERSON NAMED IN			2839.5	0.00/1
0.06647 0.07343 0.08004 0.08644 0.09886 0.11098 0.12292 0.13476 0.14653 0.15824 0.16992	2827.4 2920.8 3011.0 3100.3 3279.4 3462.4 3650.6 3844.8 4045.1	3098.3 3214.5 3831.2 3446.0 3674.9	6.5843 6.7714 6.9386	0.05842 0.06477	2818.6	Carried St. Co. Co. Co.	6,2854	0.04585	2699.0		6.2111
0.07343 0.08004 0.08644 0.09886 0.11098 0.12292 0.13476 0.14653 0.15824 0.16992	2920.8 3011.0 3100.3 3279.4 3462.4 3650.6 3844.8 4045.1	3214.5 3331.2 3446.0 3674.9	6.7714 6.9386	0.06477		3081.5	6.5158	0.05197			6.4516
0.08004 0.08644 0.09886 0.11098 0.12292 0.13476 0.14653 0.15824 0.16992	3011.0 3100.3 3279.4 3462.4 3650.6 3844.8 4045.1	3831.2 3446.0 3674.9	6.9386	# 1560 YOUR DOOR PARK WATER	2914.2	3205.7	6.7071	0.05784			6.6483
0.08644 0.09886 0.11098 0.12292 0.13476 0.14653 0.15824 0.16992	3100.3 3279.4 3462.4 3650.6 3844.8 4045.1	3446.0 3674.9	A STANSON OF THE PROPERTY OF T	17.117.1170	3005.8	3324.2	6.8770	0.06332	3000.6		6.8210
0.09886 0.11098 0.12292 0.13476 0.14653 0.15824 0.16992	3279.4 3462.4 3650.6 3844.8 4045.1	3674.9	1.00-	0.07652	3096.0	3440.4	7.0323	0.06858	3091.8		6.9781
0.11098 0.12292 0.13476 0.14653 0.15824 0.16992	3462.4 3650.6 3844.8 4045.1	A STATE OF THE PARTY OF THE PAR	7.3706	0.08766	3276.4	3670.9	7.3127	0.07870	3273.3		7.2605
9.12292 9.13476 9.14653 9.15824 9.16992	3650.6 3844.8 4045.1	020010	7.6214	0.09850	3460.0	3903.3	7.5647	0.08852	3457.7		7.5136
0.13476 0.14653 0.15824 0.16992	3844.8 4045.1	4142.3	7.8523	0.10916	3648.8	4140.0	7.7962	0.09816	3646.9	CHEST STREET,	7.7458
0.14653 0.15824 0.16992	4045.1	4383.9	8.0675	0.11972	3843.3	4382.1	8.0118	0.10769	3841.8	SERVICE STATE OF THE SERVICE S	7.9619
0.15824		4631.2	8.2698	0.13020	4043.9	4629.8	8.2144	0.11715	4042.6	11 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	8.1648
0.16992	4251.4	4884.4	8.4612	0.14064	4250.4	4888.2	8.4060	0.12655	4249.3	Strike of the Authority Strategy	8.3566
CONTRACTOR OF THE PARTY OF THE	4463.5	5143.2	8.6480	0.15103	4462.6	5142.2	8.5880	0.13592	4461.6	GENERAL BUT MARCHA	8.5388
	4680.9	5407.2	8.8164	0.16140	4680.1	5405.5	8,7616	0.14527	4679.3	EDD IN THE PARTY OF THE PARTY O	8,7124
0.18157		Shirk district	and entire Linear	ASSESSED TO SE		COLUMN TO SERVICE STATE OF THE		For III - Chicago	A STATE OF THE PARTY OF THE PAR	TENTAL COL	LES ELLES
ρ:	= 6.0 MPa	COLUMN TO SERVICE	Marian Table	WO-SHARWAN AND ASSESSMENT	DAVID SECTION S	(285.83°C	Million Statement	SSXXXIII STATE	8.0 MPa	No. of Street, or other Designation of the London	SET STATE OF STREET
0.03245	2589.9	2784.6	5.8902	0.027378		2772.6	5.8148	0.023525			5.7450
0.03619	2668.4	2885.6	6.0708	0.029492		2839.9	5.9337	0.024279			5.7937
0.04225	2790.4	3043.9	6.3357	0.035262		3016.9	6.2305	0.029975			6.1321
0.04742	2893.7	3178.3	6.5432	0.039958		3159.2	6.4502	0.034344			6.3658
0.05217	2989.9	3302.9	6.7219	0.044187	NUMBER OF SCHOOL	3288.3	6.6353	0.038194			6.5579
0.05667	3083.1	3423.1	6.8826			3411.4	6.8000				6,726
0.06102	3175.2	3541.3	7.0308	0.051966	3167.9						CONTRACTOR AMERICA
0.06527	3267.2	3658.8	7.1693								
0.07355	3453.0	3894.3	7.4247	WHATE TORING STREET, AND ADDRESS OF A PARTY	andoren, sangantesione	CONTRACTOR A TEMPORAR AND A	GATETY RESIDENCE ALTHOUGH				
0.08165	3643.2	4138.1	7.6582								
0.08964	3838.8	4376.6	7.8751			METHOD WITH MITCHES	CONTRACTOR OF THE PARTY OF THE				
0.09756	4040.1	4625.4	8.0786			STATE OF THE PERSON NAMED IN COLUMN TWO IS NOT THE OWNER.					
0.10543	4247.1	4879.7	8.2709			MIN C. 155. 1. 9 27 1.	THE RESERVE OF THE PARTY OF THE				
0.11326	4459.8	5139.4	8.4534				THE RESERVE OF THE PERSON OF T				
0.12107	4677.7	5404.1	8,6273	0.103781	4676.1	5402.6	8.5561	0.090817	46/4.5	5401.0	1 8,492
Р	= 9.0 MP	a (303,35	(0°	P :	= 10.0 MF	a (311.00	°C)	P =	12.5 MPa	(327.8	1°C)
STATE OF STREET	OF THE RESIDENCE	2742.9	5.6791	0.018028	3 2545.2	2725.5	5.6159	0.013496	2505.6	2674.3	3 5.463
0.02328	4 2647.6	2857.1	5.8738	0.019877	7 2611.6	2810.3	Supplemental Supplemental	HAD SEED A			
0.02581	6 2725.0	2957.3	6.0380	0.022440	2699.6	2924.0	5.9460				
		3118.8	6.2876	0.026436	5 2833.1	3097.5	6.2141				0 6.043
CONTRACTOR OF THE PARTY OF THE	AND THE RESERVE OF THE PARTY OF	A STATE OF THE PARTY OF THE PAR	6.4872	0.029782	2 2944.5	3242.4	6.4219	0.02301	9 2913.7	3201.	5 6.274
PERCENT PROSPERSORS	A STATE OF THE PARTY OF THE PAR	3387.4	6.6603				6.5995				6 6.465
			6.8164				6.7585				
	THE PARTY OF THE	160000110000000000000000000000000000000	6.9605				6.9045				6 6.782
COLUMN TO SERVICE STATE OF THE PARTY OF THE		The last present the last of the	7.0954				7.0408	0.03249	1 3324.1	3730.	2 6.922
THE RESERVE THE PARTY NAMED IN		Laboratory to	7.2229				7.1693				
			7.4606				7.4085				
			\$25 AL STATEMENT AND				COMPANY AND STREET	THE RESERVE THE PROPERTY OF			9 7.519
			TOWNS TO PERSON AND ADDRESS OF THE PERSON AN				7.8349				.5 7.726
C. Probable							THE SHAPE THE PARTY OF THE PART	O OFOEN	ב מכמו ח	ADCA	5 7 000
	mp 447 664 5 /			0.00010	J 4230.3	487.0.3	8.0289				.5 7.922
0.07022	2 4454.2			BE THERE MAKEN GREEN	8 4452.4	W-840000001125			2 4447.7	5127.	.0 8.106 .1 8.281
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