系所組別:化學工程系碩士班 科 目:工程數學與輸送現象

(總分為100分;所有試題務必於答案卷內頁依序作答,否則不予計分)

- 1. (38%) A naphthalene (MW=128 g/mol) sphere is kept at a uniform temperature of 27°C and is suspended in still air at 1 atm (1× 10^5 Pa) by a fine wire. The initial radius r_1 = 2.00 mm. The saturated vapor pressure of naphthalene at 27°C is P_{A1} =0.6 mmHg, and the density of solid naphthalene is 1.14 g/cm³. The diffusivity of naphthalene in the air is $7x10^{-6}$ m²/s. The gas constant, R, is 8.314 $\frac{1}{\text{mol-K}}$.
 - (a) (10%) Derive the evaporation rate (kg/s) of naphthalene and explain the assumptions you made to simplify the governing equation.
 - (b) (18%) Derive the profile of pa.
 - (c) (10%) What is the time for the completed evaporation of this naphthalene sphere?
- 2. (12%) Choose the CORRECT one(s) from the following descriptions.
 - (a) In a backward-feed multiple-effect evaporator, the high temperatures in the early effects reduce the viscosity, resulting in good heat and mass transfer.
 - (b) The percentage humidity is defined as the actual vapor pressure of water in the air divided by the water vapor pressure which is saturated at the same temperature.
 - (c) The bound moisture in solids has lower vapor pressure than water at the same temperature.
 - (d) In the design of distillation tower, the q line represents heat condition of the feed, and q is defined as q = (molar latent heat of feed vaporization)/(heat needed to vaporize 1 mol of feed at entering conditions)
 - (e) The reflux of distillation increases the purity of the overhead product, and decreases the energy cost.
 - (f) After the break-point time is reached in an adsorption bed, the solute concentration rises very rapidly, and the bed is then judged ineffective soon.

3. **(30%)**

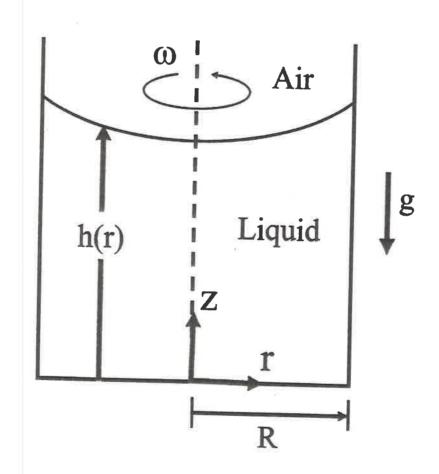
- (5%) (a) In fluid mechanics, Newton's viscosity law is mainly used to describe the relationship between fluid velocity gradient and shear stress. Consider a one-dimensional flow, if the flow direction of the fluid is in the r direction, and the direction of momentum transport is in the z direction, please write the corresponding Newton's viscosity law.
- (5%) (b) The shear stress can be regarded as the flux of which physical quantity?
- (5%) (c) Stream function (Ψ) is useful for flow visualization. It applies to incompressible two-dimensional flow situation. For example, consider a two-dimensional x-y flow in Cartesian rectangular coordinates, we can find the relationship between (v_x, v_y) and Ψ by using continuity equation as following:

系所組別:化學工程系碩士班 科 目:工程數學與輸送現象

(總分為100分;所有試題務必於答案卷內頁依序作答,否則不予計分)

Now, we consider the flow pattern in r- θ plane of spherical coordinates. Please find the relationship between (v_r, v_{θ}) and Ψ .

(15%) (d) The following figure shows a system with a gas-liquid interfaces, consisting of a liquid in an open container of radius R that is rotated at a constant angular velocity ω. Please determine the steady interface height, h(r), assuming that the ambient air pressure is P₀ and the initial volume of the liquid in the tank is V₀.





4. (20%) Please answer the following questions.

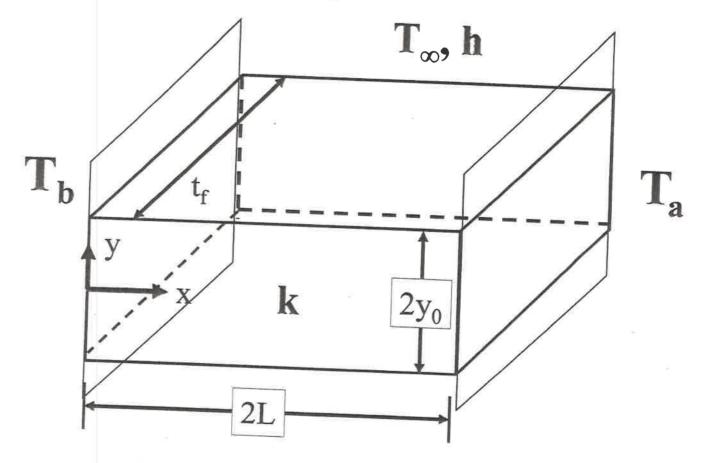
- (5%) (a) Fourier law of heat conduction can be expressed as $\frac{q}{A} = -k\nabla T$. Please explain the physical meaning of negative symbol "-".
- (15%) (b) Consider a two-dimensional heat transfer in x-y plane as shown in following figure. The temperatures of the right-hand side and left-hand side are T_a and T_b, respectively. Consider the thermal conductivity, the width and the thickness of the fin are k, t_f and

系所組別:化學工程系碩士班

目:工程數學與輸送現象

(總分為100分;所有試題務必於答案卷內頁依序作答,否則不予計分)

 $2y_0$. The temperature and heat transfer coefficient of the ambient are T_∞ and h. Please find the temperature distribution in x-y plane. [Hint: please use the definition of dimensionless temperature $\theta = \frac{T - T_b}{T_\infty - T_b}$ to solve this problem]





系所組別:化學工程系碩士班 科 目:工程數學與輸送現象

(總分為100分;所有試題務必於答案卷內頁依序作答,否則不予計分)

Supporting materials

(a) Continuity equation

$$\begin{split} &\frac{\partial \rho}{\partial t} + \nabla \bullet \rho \vec{v} = 0 \\ &\frac{\partial \rho}{\partial t} + \frac{\partial}{\partial x} (\rho v_x) + \frac{\partial}{\partial y} (\rho v_y) + \frac{\partial}{\partial z} (\rho v_z) = 0 \text{ (Cartesian rectangular coordinates)} \\ &\frac{\partial \rho}{\partial t} + \frac{1}{r} \frac{\partial}{\partial r} (\rho r v_r) + \frac{1}{r} \frac{\partial}{\partial \theta} (\rho v_\theta) + \frac{\partial}{\partial z} (\rho v_z) = 0 \text{ (Cylindrical coordinates)} \\ &\frac{\partial \rho}{\partial t} + \frac{1}{r^2} \frac{\partial}{\partial r} (\rho r^2 v_r) + \frac{1}{r \sin \theta} \frac{\partial}{\partial \theta} (\rho v_\theta \sin \theta) + \frac{1}{r \sin \theta} \frac{\partial}{\partial \phi} (\rho v_\phi) = 0 \text{ (Spherical coordinates)} \end{split}$$

(b) Navier-Stokes equation

$$\rho \frac{D\vec{v}}{Dt} = -\nabla P + \mu \nabla^2 \vec{v} + \rho \vec{g}$$

Cartesian Rectangular coordinates

$$\begin{split} \rho \left(\frac{\partial v_x}{\partial t} + v_x \frac{\partial v_x}{\partial x} + v_y \frac{\partial v_x}{\partial y} + v_z \frac{\partial v_x}{\partial z} \right) &= -\frac{\partial P}{\partial x} + \mu \left(\frac{\partial^2 v_x}{\partial x^2} + \frac{\partial^2 v_x}{\partial y^2} + \frac{\partial^2 v_x}{\partial z^2} \right) + \rho g_x \\ \rho \left(\frac{\partial v_y}{\partial t} + v_x \frac{\partial v_y}{\partial x} + v_y \frac{\partial v_y}{\partial y} + v_z \frac{\partial v_y}{\partial z} \right) &= -\frac{\partial P}{\partial y} + \mu \left(\frac{\partial^2 v_y}{\partial x^2} + \frac{\partial^2 v_y}{\partial y^2} + \frac{\partial^2 v_y}{\partial z^2} \right) + \rho g_y \\ \rho \left(\frac{\partial v_z}{\partial t} + v_x \frac{\partial v_z}{\partial x} + v_y \frac{\partial v_z}{\partial y} + v_z \frac{\partial v_z}{\partial z} \right) &= -\frac{\partial P}{\partial z} + \mu \left(\frac{\partial^2 v_y}{\partial x^2} + \frac{\partial^2 v_y}{\partial y^2} + \frac{\partial^2 v_y}{\partial z^2} \right) + \rho g_y \end{split}$$

Cylindrical coordinates

$$\begin{split} \rho \left(\frac{\partial v_{r}}{\partial t} + v_{r} \frac{\partial v_{r}}{\partial r} + \frac{v_{\theta}}{r} \frac{\partial v_{r}}{\partial \theta} + v_{z} \frac{\partial v_{r}}{\partial z} - \frac{v_{\theta}^{2}}{r} \right) &= -\frac{\partial P}{\partial r} + \mu \left[\frac{\partial}{\partial r} \left(\frac{1}{r} \frac{\partial}{\partial r} (rv_{r}) \right) + \frac{1}{r^{2}} \frac{\partial^{2} v_{r}}{\partial \theta^{2}} + \frac{\partial^{2} v_{r}}{\partial z^{2}} - \frac{2}{r^{2}} \frac{\partial v_{\theta}}{\partial \theta} \right] + \rho g_{r} \\ \rho \left(\frac{\partial v_{\theta}}{\partial t} + v_{r} \frac{\partial v_{\theta}}{\partial r} + \frac{v_{\theta}}{r} \frac{\partial v_{\theta}}{\partial \theta} + v_{z} \frac{\partial v_{\theta}}{\partial z} + \frac{v_{r}v_{\theta}}{r} \right) &= -\frac{1}{r} \frac{\partial P}{\partial \theta} + \mu \left[\frac{\partial}{\partial r} \left(\frac{1}{r} \frac{\partial}{\partial r} (rv_{\theta}) \right) + \frac{1}{r^{2}} \frac{\partial^{2} v_{\theta}}{\partial \theta^{2}} + \frac{\partial^{2} v_{\theta}}{\partial z^{2}} + \frac{2}{r^{2}} \frac{\partial v_{r}}{\partial \theta} \right] + \rho g_{\theta} \\ \rho \left(\frac{\partial v_{z}}{\partial t} + v_{r} \frac{\partial v_{z}}{\partial r} + \frac{v_{\theta}}{r} \frac{\partial v_{z}}{\partial \theta} + v_{z} \frac{\partial v_{z}}{\partial z} \right) &= -\frac{\partial P}{\partial z} + \mu \left[\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial v_{z}}{\partial r} \right) + \frac{1}{r^{2}} \frac{\partial^{2} v_{z}}{\partial \theta^{2}} + \frac{\partial^{2} v_{r}}{\partial z^{2}} \right] + \rho g_{z} \end{split}$$