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國立臺灣大學 105 學年度碩士班招生考試試題

科目:單操與輸送

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## **Useful Equations**

$$N_{Nu} = 2.0 + 0.6 N_{Re}^{0.5} N_{Pr}^{1/3}$$

Prandtl number at room temperature = 0.71

Air density  $= 1.20 \text{ kg/m}^3$ 

viscosity  $= 1.80*10^{-5} \text{ kg/m s}$ 

conductivity = 0.025 W/m K

Stefan-Boltzmann constant =  $5.67*10^{-8} \text{ W/m}^2$ 

## Henderson equation

 $1 - rh = exp(-cTM_e^n)$ 

rh = relative humidity (decimal)

T = temperature 'C

 $c = 5.78*10^{-5}$ 

n = 1 52

Me = equilibrium moisture content dry basis (%)

## Conduction Heat Transfer in a Sphere

Bi->∞

$$\frac{T - T_{\infty}}{T_i - T_{\infty}} = 1 - \frac{6}{\pi} \sum_{n=1}^{\infty} \frac{1}{n^2} \exp(-\alpha n^2 \pi^2 t/r^2)$$

Ti = initial temperature

T∞ = surface temperature

 $\alpha$  = thermal conductivity

r = radius

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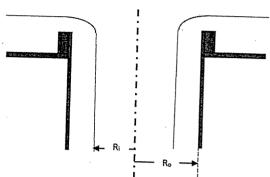
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1. As shown schematically figure below, a viscos fluid flow over a weir at the end of



a circular tube to form an annular flow in the tube and into a storage tank. Develop a mathematical model to explain why there are bubbles continuously arising from the liquid in the tanks.

- a. Write the models in differential equations with boundary conditions, clearly
  define all variables used in the models with appropriate dimensions in SI units.
  You don't have to solve those equations for credits. (15 points)
- b. If the flow rate of viscos fluid is known, explain how to estimate the amount of air flowing into the tanks. (5 points)
- 2. A sphere with radius 0.25 m at 37 °C is enclosed in the center of a spherical shell with radius 5 m at 5 °C, air in the shell is stationary at 10 °C. Calculate heat loss from the sphere in the shell. Write your major assumptions in your procedure. (20 points)
- 3. A soybean kernel diameter 8mm, density  $1100 \text{ kg/m}^3$  (moisture contain 20% wet basis) is continuously drying in hot air. If it is a falling rate drying and moisture migrating in the kernel follows Fick's law with moisture diffusivity  $D = 2.0 * 10^{-10} \text{ m}^2/\text{s}$ . Moisture at the soybean surface equilibrium with hot air instantaneously. Equilibrium moisture content of soybean can be predicted from Henderson equation.
- a. An air stream having a dry-bulb temperature of 20.5 °C and wet-bulb temperature 18 °C being heated through a heat exchanger to 45 °C is used in soybean drying. What is the equilibrium moisture content of soybean in the hot airstream? (10 points)
- Try to estimate the final moisture contain in wet basis after 30 min of drying. (10 points)

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4. A continuous single-effect evaporator concentrates 10800kg/h of a 1.0 wt% salt solution entering at 30°C to a final concentration of 1.5 wt%. The vapor space of the evaporator is at 70.14kPa and the steam supplied is saturated at 143.3kPa. The overall coefficient U = 2000 W/m²K. Calculate the amounts of vapor and liquid product and heat-transfer area required, Assume that, since it is dilute, the solution has the same boiling point and enthalpy as water. (20 points)

5. A continuous deodorizing system, involving a single stage steam stripping operation, is under consideration for the removal of a taint from cream. If the taint component is present in the cream to the extent of 8 parts per million (ppm) and if steam is to be passed through the contact stage in the proportions of 0.75 kg steam to every 1 kg cream, calculate the concentration of the taint in the leaving cream. The equilibrium concentration distribution of the taint has been found experimentally to be in the ratio of 1 in the cream to 10 in the steam and it is assumed that equilibrium is reached in each stage. (20 points)

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A.2-9 Properties of Saturated Steam and Water (Steam Table), SI Units

Temper- ature	re Pressi	re vii (ky)			Enthalpy (kJ/kg)		Entropy (kJ/kg·K)	
(*0		Liquid	Sat'd Vaj	or Liquid	Sat'd Vap			
	.01 0.6	113 0.0010002	206.136	0.00	2504			
3	0.7:	577 0.0010001	168.132	12.5		0.000		
6	0.93	349 0.0010001	137.734	25.20		0,0457	~~~	
9	1.14	177 0.0010003	113.386	37.80		0.0912		
12	1.40	0.0010005	93.784	50.41		0.1362		
15	1.70		77.926	62.99		0.1806	~ ~~~	
18	2.06	The state of the s	65.038	75.58		0.2245	1 m	
21	2.48		54.514	88.14		0.2679		
24	2.98	5 0.0010027	45.883	100.70		0.3109	8.6450	
25	3.16	9 0.0010029	43.360	,104.89	2545,4 2547.2	0.3534	8.5794	
27	3.56	7 0.0010035	38.774	113.25	2347.2	0.3674	8.5580	
30	4.24	6 0.0010043	32.894	125.79	2550,8	0.3954	8.5156	
. 33	5.03	0.0010053	28.011	138.33	2556.3	0.4369	8,4533	
36	5.94	0.0010063	23.940	150.86	2561.7	0.4781	8.3927	
40	7,384	0.0010078	19.523	167.57	2567.1	0.5188	8,3336	
45	9,593	0.0010099	15,258	188.45	2574,3	0.5725	8.2570	
50	12.349	0.0010121	12.032	209,33	2583.2	0.6387	8.1648	
55	15,758	0.0010146	9.568	230.23	2592,1	0.7038	8.0763	
60	19,940	0.0010172	7.671	251.13	2600.9	0.7679	7.9913	
65	25.03	0.0010199	6.197	272.06	2609.6	0.8312	7,9096	
70	31.19	0.0010228	5.042	292,98	2618.3	0.8935	7.8310	
75	38.58	0.0010259	4.131	313,93	2626.8	0.9549	7.7553	
80	47,39	0.0010291	3.407	334.91	2635.3	1.0155	7.6824	
85	57.83	0.0010325	2.828	355.90	2643.7	1.0753	7.6122	
90	70.14	0.0010360	2.361	376.92	2651.9	1.1343	7.5445	
95	84.55	0.0010397	1.9819	397.96	2660.1	1.1925	7.4791	
100	101,35	0.0010435	1.6729	419.04	2668,1	1.2500	7.4159	
105	120.82	0.0010475	1,4194	The state of the s	2676.1	1.3069	7.3549	
110	143.27	0.0010516	1.2102	440.15	2683.8	1.3630	7.2958	
115	169.06	0.0010559	1.0366	461,30	2691.5	1.4185	7.2387	
120	198.53	0.0010603		482.48	2699.0	1.4734	7.1833	
125	232.1	0.0010649	0.8919	503.71	2706.3	1.5276	7.1296	
130	270.1	0.0010697	0.7706	524.99	2713.5	1.5813	7.0775	
135	313.0	0.0010746	0.6685	546.31	2720.5	1,6344	7.0269	
140	316.3	0.0010797	0.5822	567.69	2727.3	1.6870	6.9777	
45	415.4	0.0010797	0,5089	589.13	2733.9	1.7391	6.9299	
50	475.8	0.0010905	0.4463	610.63	2740.3	1.7907	6.8833	
55	543.1	0.0010961	0.3928	632.20	2746.5	1.8418	6.8379	
60	617.8	0.0010301	0.3468	653.84	2752.4	1.8925	6.7935	
65	700.5	0.0011020	0.3071	675.55	2758.1	1.9427	6.7502	
70	791.7	0.0011143	0.2727	697.34		1.9925	6.7078	
75	892.0	0.0011143	0.2428	719.21		2.0419	6.6663	
80	1002.1	0.0011207	0.2168	741.17		2.0909	6.6256	
90	1254,4	0.0011274	0.19405	763.22		2,1396	6.5857	
00	1553.8	0.0011414	0.15654	807.62	Carlotte and the Control	2.2359	6.5079	
25	2548	0.0011363	0.12736	852.45		2.3309	6.4323	
50	3973	0.0011992	0.07849			2.5639	6.2503	
100	5942	0.0012512		1085.36		2.7927	6.0730	
	8581	0.0013168		1210.07	2785.0		5,8938	
7.27	77.000.000	A-0010430	0.02167	1.344.0	2749.0 🧠 3		5.7045	

Source: Abridged from J. H. Keenan, F. G. Keyes, P. G. Hill, and J. G. Moore, Steam Tables - Metric Units. New York: John Wiley & Sons, Inc., 1969. With permission of the authors and publishers.

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