

## 淡江大學 103 學年度碩士班招生考試試題

系別：化學工程與材料工程學系

科目：輸送現象與單元操作

考試日期：3月2日(星期日) 第2節

本試題共4大題，2頁

1. A constant density, Newtonian fluid flows steadily between two infinite, parallel plates as shown in Fig. 1. The bottom plate is stationary and the top plate (at  $z=h$ ) is moving steadily in the  $x$  direction with velocity 'A'. The gravity is not important.

- (1) Please solve the pressure profile with all the assumptions and boundary conditions clearly stated. (15%)
- (2) Please solve the velocity profile with all the assumptions and boundary conditions clearly stated. (15%)

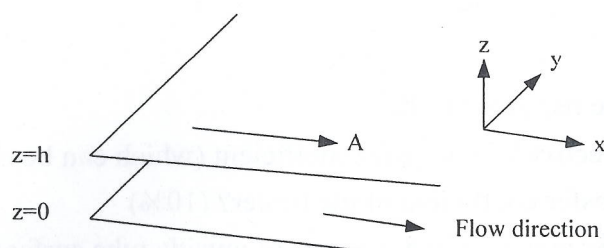


Fig. 1

Equation of continuity:

$$\frac{\partial \rho}{\partial t} + \frac{\partial(\rho v_x)}{\partial x} + \frac{\partial(\rho v_y)}{\partial y} + \frac{\partial(\rho v_z)}{\partial z} = 0.$$

Equation of motion for a constant density and Newtonian fluid:

$$\rho \left( \frac{\partial v_x}{\partial t} + v_x \frac{\partial v_x}{\partial x} + v_y \frac{\partial v_x}{\partial y} + v_z \frac{\partial v_x}{\partial z} \right) = -\frac{\partial p}{\partial x} + \mu \left( \frac{\partial^2 v_x}{\partial x^2} + \frac{\partial^2 v_x}{\partial y^2} + \frac{\partial^2 v_x}{\partial z^2} \right) + \rho g_x,$$

$$\rho \left( \frac{\partial v_y}{\partial t} + v_x \frac{\partial v_y}{\partial x} + v_y \frac{\partial v_y}{\partial y} + v_z \frac{\partial v_y}{\partial z} \right) = -\frac{\partial p}{\partial y} + \mu \left( \frac{\partial^2 v_y}{\partial x^2} + \frac{\partial^2 v_y}{\partial y^2} + \frac{\partial^2 v_y}{\partial z^2} \right) + \rho g_y,$$

$$\rho \left( \frac{\partial v_z}{\partial t} + v_x \frac{\partial v_z}{\partial x} + v_y \frac{\partial v_z}{\partial y} + v_z \frac{\partial v_z}{\partial z} \right) = -\frac{\partial p}{\partial z} + \mu \left( \frac{\partial^2 v_z}{\partial x^2} + \frac{\partial^2 v_z}{\partial y^2} + \frac{\partial^2 v_z}{\partial z^2} \right) + \rho g_z.$$

2. It is known that for fully developed turbulent flow in conduits with  $Re > 10000$ ,  $0.7 < Pr < 160$ , and  $L/d > 60$ , the following Chilton-Colburn analogy can be applied.

$$J_M = \frac{f}{2} = J_H = \frac{Nu}{Re Pr^{1/3}} = J_D = \frac{Sh}{Re Sc^{1/3}}$$

$$\left( f = \frac{\tau_w}{\frac{1}{2}\rho u^2} \quad Nu = \frac{hd}{k_c} \quad Re = \frac{\rho u d}{\mu} \quad Pr = \frac{c_p \mu}{k_c} \quad Sh = \frac{kd_h}{D} \quad Sc = \frac{\mu}{\rho D} \right)$$

For the following correlation (Eq. (1)) commonly adopted for convective heat transfer through conduit wall in the turbulent flow regime, please suggest a correlation for estimating convective mass transfer coefficient. (10%)

$$Nu = 0.023 Re^{0.8} Pr^{\frac{1}{3}} \quad (1)$$

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4-2

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3. A tubular feedwater heater is being designed to heat 0.368 kg/s of water from 21°C to 90°C. Saturated steam at 923 kPa (176°C) is condensing on the outside of the tubes. The tubes are a copper alloy. Each tube has a 2.54 cm outside diameter and a 2.29 cm inside diameter. The water velocity inside the tubes is 0.9 m/s. For the steam outside the tube, the convective heat transfer coefficient can be assumed to be  $13600 \frac{W}{m^2 K}$ . The heat transfer resistance of the tube is negligible. (For water,  $C_p = 4.1864 \frac{kJ}{kg K}$   $\rho = 1000 \frac{kg}{m^3}$   $\mu = 0.5 \times 10^{-3} \frac{kg}{m s}$   $k_c = 0.65 \frac{W}{m K}$   $Pr=3.37$ )
- (1) What is the heat transfer rate required? (10%)
  - (2) What are the tube side convective heat transfer coefficient (which can be estimated using Eq. (1)) and the overall heat transfer coefficient of the heater? (10%)
  - (3) What is the total heat transfer area required in terms of outside tube surface area? (10%)
4. For the separation of a mixture using packed bed distillation column, the mass flux of species 'A' across the gas-liquid interface can be written as Eq. (2).
- (1) Please explain Eq. (2) based on two-film theory. A diagram must be sketched with variables marked on it. (10%)
  - (2) Please provide the definition and dimension for each variable in Eq. (2). (10%)
  - (3) Please derive Eq. (3) and define the variable 'm'. (10%)

$$\begin{aligned}
 N_A &= k_G(y_{AG} - y_{Ai}) \\
 &= k_L(x_{Ai} - x_{AL}) \\
 &= K_{OG}(y_{AG} - y_A^*) \\
 &= K_{OL}(x_A^* - x_{AL})
 \end{aligned}
 \tag{2}$$

$$\frac{1}{K_{OG}} = \frac{1}{k_G} + \frac{m}{k_L}
 \tag{3}$$